Tables

Tables Imbedded in Report

Table 4

Wells Used for Water Level Monitoring During CH-16 Aquifer Test

TABLE 4 WELLS USED FOR WATER LEVEL MONITORING DURING CH-16 AQUIFER TEST
HOFFMAN-La ROCHE INC. - NUTLEY, NJ

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16 (ft)
CH-1	8	650	Deep Bedrock	1446
CH-2	8	650	Deep Bedrock	2521
CH-3	8	450	Deep Bedrock	2618
CH-4	8	503	Deep Bedrock	2012
CH-5	8	400	Deep Bedrock	1310
CH-6	8	500	Deep Bedrock	989
CH-7	8	500	Deep Bedrock	279
CH-8	8	500	Deep Bedrock	1569
CH-9	8	425	Deep Bedrock	1560
CH-10	8	~450	Deep Bedrock	1145
CH-11	8	~450	Deep Bedrock	1218
CH-12	8	~450	Deep Bedrock	885
CH-13	8	~450	Deep Bedrock	541
CH-14	8	~450	Deep Bedrock	478
CH-15	8	~450	Deep Bedrock	873
CH-16*	8	~450	Pumping Well	0
CH-17	8	~450	Deep Bedrock	907
CH-18	8	~450	Deep Bedrock	456
CH-19	8	~450	Deep Bedrock	936
CH-20	8	~450	Deep Bedrock	158
MW-113 (CH-11)	6	80	Shallow Bedrock	1233
MW-114 (CH-12)	6	80	Shallow Bedrock	904
MW-115 (CH-13)	6	80	Shallow Bedrock	537
MW-116 (CH-14)	6	80	Shallow Bedrock	456
MW-117 (CH-15)	6	80	Shallow Bedrock	872
MW-118 (CH-16)	6	80	Shallow Bedrock	20
MW-119 (CH-17)	6	80	Shallow Bedrock	890
MW-120 (CH-18)	6	80	Shallow Bedrock	441
MW-121 (CH-19)	6	80	Shallow Bedrock	935
MW-122 (CH-20)	6	80	Shallow Bedrock	166
ML-37	10	728.5	Deep Bedrock	327
MW-1	4	14.3	Overburden/Bedrock	2048
MW-2	6	30.5	Shallow Bedrock	1592
MW-3	6	79	Shallow Bedrock	674
MW-5	6	30	Shallow Bedrock	1673
MW-6A	4	25	Shallow Bedrock	1395
MW-7A	2	15.5	Overburden	1029
MW-7C	2	30	Shallow Bedrock	1147

TABLE 4 WELLS USED FOR WATER LEVEL MONITORING DURING CH-16 AQUIFER TEST
HOFFMAN-La ROCHE INC. - NUTLEY, NJ

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16 (ft)
MW-8A	6	33	Shallow Bedrock	546
MW-10	4	14.8	Overburden/Bedrock	575
MW-12	6	50	Shallow Bedrock	412
MW-15A	2	15	Overburden	804
MW-15B	3	30	Shallow Bedrock	804
MW-18	4	19	Overburden	810
MW-19A	4	18	Overburden/Bedrock	338
MW-22A	3	45	Shallow Bedrock	1299
MW-24	6	42	Shallow Bedrock	1262
MW-26A	6	50.5	Shallow Bedrock	942
MW-33	2	23	Overburden/Bedrock	965
MW-34	2	49.3	Shallow Bedrock	580
MW-35	2	49.9	Shallow Bedrock	497
MW-36	2	49.7	Shallow Bedrock	347
MW-37	6	34.9	Shallow Bedrock	692
MW-38	2	6.5	Overburden	441
MW-39A	2	18.5	Shallow Bedrock	436
MW-39-1	4	21.5	Overburden/Bedrock	1435
MW-40A	2	39	Shallow Bedrock	433
MW-41	2	58.7	Shallow Bedrock	436
MW-42	2	17.2	Overburden/Bedrock	414
MW-43	2	24.5	Shallow Bedrock	1958
MW-46	6	62	Shallow Bedrock	512
MW-50	6	45	Shallow Bedrock	1419
MW-52	6	30	Shallow Bedrock	1444
MW-55	6	26	Shallow Bedrock	972
MW-57	6	17.5	Shallow Bedrock	1116
MW-58	2	36.7	Shallow Bedrock	2349
MW-59	6	25.5	Shallow Bedrock	1774
MW-60	2	22	Overburden/Bedrock	1362
MW-61	6	41	Shallow Bedrock	1106
MW-63	2	41.5	Shallow Bedrock	892
MW-69	4	18.2	Overburden/Bedrock	992
MW-70-1	6	35.4	Shallow Bedrock	1718
MW-72	4	20	Overburden	968
MW-73	4	22	Overburden/Bedrock	958
MW-74	6	40	Shallow Bedrock	968
MW-80	2	18.5	Overburden/Bedrock	1295

TABLE 4 WELLS USED FOR WATER LEVEL MONITORING DURING CH-16 AQUIFER TEST
HOFFMAN-La ROCHE INC. - NUTLEY, NJ

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16 (ft)
MW-81	2	20	Overburden	917
MW-103A	2	15	Overburden/Bedrock	1165
MW-103B	6	37.4	Shallow Bedrock	1162
MW-104A	2	13.3	Overburden/Bedrock	1097
MW-104B	6	33.7	Shallow Bedrock	1096
MW-105B	6	38.7	Shallow Bedrock	1380
MW-106A	2	12.3	Overburden/Bedrock	1088
MW-106B	6	33.8	Shallow Bedrock	1090
MW-107	6	32	Shallow Bedrock	1199
MW-108A	2	10.7	Overburden	1274
MW-108B	6	31.8	Shallow Bedrock	1274

Notes:

1. CH-16 was the pumping well.

Table 5

CH-16 Aquifer Test Transducer Installation Table

TABLE 5
CH-16 AQUIFER TEST TRANSDUCER INSTALLATION TABLE
HOFFMANN LA-ROCHE, NUTLEY, NEW JERSEY

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Transducer Cable Length (ft)	Transducer Rating	Distance from CH-16 (ft)	Transducer Installed Date / Time	Transducer Serial Number	Depth to Transducer (ft)	Manual Depth to Water (ft)	Transducer Reading (ft of H_2O)	Comments
CH-1	8	650	100	100 psi / 230 ft	1446	5/24/2010 12:27	163447	96.64	13.76	82.88	
CH-2	8	650	100	100 psi / 230 ft	2521	5/21/2010 14:05	131810	90.12	15.06	75.06	
CH-3	8	450	100	100 psi / 230 ft	2618	5/24/2010 13:56	136380	90.59	14.20	76.39	
CH-4	8	503	100	100 psi / 230 ft	2012	5/24/2010 14:54	120452	87.78	13.00	74.78	
CH-5	8	400	100	100 psi / 230 ft	1310	5/24/2010 12:18	149064	87.27	4.54	82.73	
CH-6	8	500	100	100 psi / 230 ft	989	5/21/2010 12:38	149724	88.55	14.35	74.20	
CH-7	8	500	100	100 psi / 230 ft	279	5/20/2012 19:42	163477	91.06	21.75	69.31	
CH-8	8	500	100	100 psi / 230 ft	1569	5/21/2010 12:28	163457	92.24	17.45	74.79	
CH-9	8	425	100	100 psi / 230 ft	1560	5/24/2010 17:18	149173	252.12	8.10	244.02	
CH-10	8	~450	150	100 psi / 230 ft	1145	5/21/2010 12:16	152578	135.80	22.26	113.54	
CH-11	8	~450	100	100 psi / 230 ft	1218	5/21/2010 12:08	163448	93.53	23.19	70.34	
CH-12	8	~450	300	100 psi / 230 ft	885	5/21/2010 11:50	163443	250.01	60.71	189.30	
CH-13	8	~450	600	100 psi / 230 ft	541	5/20/2010 18:43	163428	255.52	48.44	207.08	
CH-14	8	~450	300	100 psi / 230 ft	478	5/20/2010 19:19	163452	251.13	21.86	229.27	
CH-15	8	~450	300	100 psi / 230 ft	873	5/24/2010 12:59	163456	93.11	11.7	81.41	
CH-16*	8	~450	300	100 psi / 230 ft	0	5/24/2010 14:58	153945	250.11	51.99	198.12	
CH-17	8	~450	500	100 psi / 230 ft	907	5/21/2010 12:39	163502	258.40	7.35	251.05	
CH-18	8	~450	300	100 psi / 230 ft	456	5/20/2010 17:50	163451	206.54	48.81	157.73	
CH-19	8	~450	100	100 psi / 230 ft	936	5/24/2010 11:55	120715	248.07	42.26	205.81	
CH-20	8	~450	300	100 psi / 230 ft	158	5/20/2010 18:05	154260	193.52	55.00	138.52	
MW-113 (CH-11)	6	80	75	30 psi / 70 ft	1233	5/21/2010 12:05	117673	71.87	16.71	55.16	
MW-114 (CH-12)	6	80	75	30 psi / 70 ft	904	5/21/2010 11:45	124200	77.79	45.13	32.66	
MW-115 (CH-13)	6	80	75	30 psi / 70 ft	537	5/20/2010 18:49	149891	77.75	34.95	42.80	
MW-116 (CH-14)	6	80	75	30 psi / 70 ft	456	5/20/2010 19:23	118870	71.82	10.60	61.22	
MW-117 (CH-15)	6	80	70	100 psi / 230 ft	872	5/24/2010 13:02	149013	68.10	10.73	57.37	
MW-118 (CH-16)	6	80	75	30 psi / 70 ft	20	5/20/2010 18:13	108874	77.43	53.28	24.15	
MW-119 (CH-17)	6	80	100	100 psi / 230 ft	890	5/21/2010 12:30	115534	73.38	7.64	65.74	
MW-120 (CH-18)	6	80	75	30 psi / 70 ft	441	5/20/2010 17:55	135140	77.02	48.59	28.43	
MW-121 (CH-19)	6	80	75	30 psi / 70 ft	935	5/24/2010 14:49	150036	78.13	19.19	58.94	
MW-122 (CH-20)	6	80	75	30 psi / 70 ft	166	5/21/2010 11:10	118898	78.96	55.80	23.16	
PW-37	10	728.5	NA	NA	327	NA	NA	NA	NA	NA	Multilevel Flute Installed
MW-1	4	14.3	15	15 psi / 35 ft	2048	5/19/2010 18:55	133421	12.58	3.72	8.86	
MW-2	6	30.5	50	15 psi / 35 ft	1592	5/24/2010 13:30	163724	27.57	5.22	22.35	
MW-3	6	79	75	30 psi / 70 ft	674	5/19/2010 18:35	149852	74.21	48.10	26.11	
MW-5	6	30	50	15 psi / 35 ft	1673	5/24/10 12:41	163713	27.01	6.30	20.71	
MW-6A	4	25	25	15 psi / 35 ft	1395	5/24/10 12:23	163750	20.74	9.11	11.63	
MW-7A	2	15.5	15	15 psi / 35 ft	1029	5/24/10 11:59	132964	12.68	7.41	5.27	
MW-7C	2	30	50	15 psi / 35 ft	1147	5/24/10 12:34	163694	23.89	9.22	14.67	
MW-8A	6	33	50	15 psi / 35 ft	546	5/24/10 13:11	163677	30.82	17.12	13.70	
MW-10	4	14.8	15	15 psi / 35 ft	575	5/20/2010 19:14	151736	12.56	6.75	5.81	
MW-12	6	50	50	30 psi / 70 ft	412	5/20/2010 18:28	150014	38.59	18.50	20.09	
MW-15A	2	15	15	15 psi / 35 ft	804	5/24/10 12:52	127366	12.42	8.50	3.92	
MW-15B	3	30	25	15 psi / 35 ft	804	5/24/10 12:55	163679	22.64	9.15	13.49	
MW-18	4	19	25	15 psi / 35 ft	810	5/24/10 12:04	163831	15.91	8.49	7.42	
MW-19A	4	18	25	15 psi / 35 ft	338	5/24/10 13:59	163762	15.18	10.25	4.93	
MW-22A	3	45	50	30 psi / 70 ft	1299	5/24/10 12:30	125949	41.95	9.00	32.95	
MW-24	6	42	50	30 psi / 70 ft	1262	5/19/2010 18:15	118882	23.75	11.41	12.34	
MW-26A	6	50.5	50	30 psi / 70 ft	942	5/24/10 11:56	142677	45.75	8.65	37.10	
MW-33	2	23	25	15 psi / 35 ft	965	5/24/10 11:38	163761	20.37	10.07	10.30	
MW-34	2	49.3	50	15 psi / 35 ft	580	5/20/2010 18:58	163723	47.84	35.29	12.55	
MW-35	2	49.9	50	15 psi / 35 ft	497	5/20/2010 18:38	117918	48.27	35.48	12.79	
MW-36	2	49.7	50	15 psi / 35 ft	347	5/21/10 11:41	163433	47.50	9.86	37.64	
MW-37	6	34.9	40	15 psi / 35 ft	692	5/24/2010 13:18	163683	32.32	19.48	12.84	
MW-38	2	6.5	15	15 psi / 35 ft	441	5/20/2010 19:28	130790	6.545	5.72	0.825	
MW-39A	2	18.5	25	15 psi / 35 ft	436	5/21/2010 11:53	163965	16.47	7.73	8.74	
MW-40A	2	39	50	15 psi / 35 ft	433	5/21/2010 12:01	163189	36.7	8.71	27.99	
MW-41	2	58.7	75	30 psi / 70 ft	436	5/21/2010 12:05	128768	56.07	10.30	45.77	
MW-42	2	17.2	15	15 psi / 35 ft	414	5/20/2010 19:36	152123	15.01	9.02	5.99	
MW-43	2	24.5	25	15 psi / 35 ft	1958	5/24/2010 15:32	119359	23.00	12.11	10.89	
MW-46	6	62	70	15 psi / 35 ft	512	5/21/2010 11:28	131750	57.85	49.57	8.28	
MW-50	6	45	50	30 psi / 70 ft	1419	5/24/2010 12:19	149860	42.30	9.61	32.69	
MW-52	6	30	50	15 psi / 35 ft	1444	5/24/2010 12:14	163972	27.10	10.85	16.25	
MW-55	6	26	25	15 psi / 35 ft	972	5/24/2010 12:05	163968	23.81	11.82	11.99	
MW-57	6	17.5	15	15 psi / 35 ft	1116	5/24/2010 11:39	145926	13.97	8.24	5.73	
MW-59	6	25.5	25	15 psi / 35 ft	1774	5/24/2010 12:15	163074	22.95	13.82	9.13	
MW-60	2	22	25	15 psi / 35 ft	1362	5/24/2010 11:44	163967	17.71	11.11	6.60	
MW-61	6	41	50	15 psi / 35 ft	1106	5/24/2010 11:35	163240	37.77	28.49	9.28	
MW-63	2	41.5	50	30 psi / 70 ft	892	5/24/2010 11:24	108870	38.97	7.77	31.20	
MW-69	4	18.2	15	15 psi / 35 ft	992	5/24/2010 11:51	117818	15.55	8.62	6.93	
MW-70-1	6	35.4	50	30 psi / 70 ft	1718	5/24/2010 17:25	114983	31.74	4.12	27.62	
MW-72	4	20	25	15 psi / 35 ft	968	5/24/2010 11:30	163248	17.41	9.75	7.66	
MW-73	4	22	25	15 psi / 35 ft	958	5/24/2010 11:45	163969	19.35	9.17	10.18	
MW-74	6	40	50	30 psi / 70 ft	968	5/24/2010 11:33	118516	37.54	9.42	28.12	
MW-80	2	18.5	15	15 psi / 35 ft	1295	5/19/2010 17:55	163754	14.04	11.47	2.57	
MW-81	2	20	70	15 psi / 35 ft	917	5/24/2010 14:31	160780	16.89	12.03	4.86	
MW-103A	2	15	25	15 psi / 35 ft	1165	5/21/2010 11:59	117768	12.97	6.21	6.76	
MW-103B	6	37.4	50	30 psi / 70 ft	1162	5/21/2010 12:06	156493	35.47	2.57	32.9	
MW-104A	2	13.3	15	15 psi / 35 ft	1097	5/21/2010 12:41	146197	12.36	5.97	6.39	
MW-104B	6	33.7	50	30 psi / 70 ft	1096	5/21/2010 12:46	124198	32.12	5.07	27.05	
MW-105B	6	38.7	50	30 psi / 70 ft	1380	5/20/2010 19:14	125956	36.50	2.12	34.38	
MW-106A	2	12.3	15	15 psi / 35 ft	1088	5/20/2010 18:09	137411	11.50	6.37	5.13	
MW-106B	6	33.8	50	30 psi / 70 ft	1090	5/20/2010 18:17	118891	31.28	3.97	27.31	
MW-107	6	32	50	30 psi / 70 ft	1199	5/20/2010 19:47	142500	30.00	5.39	24.61	
MW-108A	2	10.7	15	15 psi / 35 ft	1274	5/20/2010 16:53	122791	9.70	5.98	3.719	
MW-108B	6	31.8	50	30 psi / 70 ft	1274	5/20/2010 18:40	124215	29.94	3.70	26.24	

Table 7

Pumping Test Collection Schedule

TABLE 7 - PUMPING TEST SAMPLE COLLECTION SCHEDULE
HOFFMANN LA-ROCHE, NUTLEY, NEW JERSEY

ANALYSES FOR GROUNDWATER CHARACTERIZATION

Analytical Parameter	Analytical Method	0 to 1 Hour of Pumping	24 Hours of Pumping	48 Hours of Pumping	72 Hours of Pumping
VOCs (+hexane/ethyl ether) + TICs	EPA 8260 B	X	X	X	X
BNAs (+pyridine) + TICs	EPA 8270 C	X	X	X	X
Select Metals*	EPA 200.7/245.1	X	X	X	X
*As, Al, Cd, Cr, Cu, Pb, Hg, Mn, Ni, Zn					
Temperature	In-situ, temperature probe	Collected every 4 hours			
Dissolved Oxygen (DO)	In-situ, DO meter	Collected every 4 hours			
Conductivity	In-situ, conductivity probe	Collected every 4 hours			
Redox (Eh)	In-situ, ORP probe	Collected every 4 hours			
pH	In-situ, pH probe	Collected every 4 hours			

ANALYSES FOR TREATMENT SYSTEM DESIGN

Analytical Parameter	Analytical Method	0 to 1 Hour of Pumping	24 Hours of Pumping	48 Hours of Pumping	72 Hours of Pumping
Ammonia (as nitrogen)	EPA 350.1				X
Manganese (II & IV)	EPA 200.7 (Total & Filtered)/Mod 7199				X
Iron (II & III)	General Method 3500-Fe D				X
Na	EPA 200.7 (ICP)				X
Mo	EPA 200.7				X
Total Phenol	EPA 420.1				X
Oil and Grease	EPA 413.2				X
Total Phosphorus	EPA 365.2				X
Soluble Organic Carbon	EPA 415.1				X
Alkalinity (total as CaCO3)	EPA 310.1				X
TDS	EPA 160.1				X
TSS	EPA 160.2				X
COD	EPA 410.3				X
Hardness (total as CaCO3)	EPA 130.2				X
Nitrate	EPA 353.2				X
Nitrite	EPA 353.2				X
Sulfide	EPA M. 376.1				X
Sulfate	EPA 375.1				X
Cl	EPA 325.3				X

Notes:
1.) Samples are of pre-treatment water and are collected between well head and first collection/treatment component

2.) Turbidity analysis are conducted for post-treatment aqueous samples

3.) Ferrous iron and Manganese (Fe-Mn II) are dissolved and are field filtered prior to preservation

Table 8

Barometric Efficiency Summary Table

Table 8
Barometric Efficiency Summary Table

Well ID	Run	Barometric Efficiency	Ave. BE	BE Applied	Trend Equation[1]	R^2	Time Period		Comments
							Start	End	
CH-1	1	0.4100	-	-	WL = 0.4105(BP_a) + 68.869	0.6247	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	2	0.4400	-	-	WL = 0.4408(BP_a) + 67.818	0.7239	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
CH-2	1	-0.6994			WL = -0.6994(BP_a) + 99.149	0.7389	May 21, 2010 0900	May 23, 2010 1500	
	2	-0.9065	-0.855	-0.855	WL = -0.9065(BP_a) + 106.18	0.6805	May 23, 2010 1500	May 25, 2010 1500	
	3	-0.9597			WL = -0.9597(BP_a) + 108.04	0.7410	May 21, 2010 0900	May 24, 2010 1500	
CH-3	1	0.1500	-	-	WL = 0.1502(BP_a) + 71.248	0.1409	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
	2	0.0030	-	-	WL = 0.0038(BP_a) + 76.235	0.0003	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
CH-4	1	-0.8614	-0.832	-0.832	WL = -0.8614(BP_a) + 104.35	0.7153	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.8028			WL = -0.8028(BP_a) + 102.36	0.7067	May 21, 2010 0900	May 24, 2010 1500	
CH-5	1	-0.7050	-0.717	-0.717	WL = -0.705(BP_a) + 106.95	0.6682	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.7281			WL = -0.7281(BP_a) + 107.76	0.7163	May 21, 2010 0900	May 24, 2010 1500	
CH-6	1	-0.7885	-0.719	-0.719	WL = -0.7885(BP_a) + 101.13	0.8727	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.6503			WL = -0.6503(BP_a) + 96.411	0.7838	May 21, 2010 0900	May 24, 2010 1500	
CH-7	1	-0.5160	-	-	WL = -0.516(BP_a) + 87.316	0.5277	May 23, 2010 1500	May 24, 2010 1500	
	2	0.5360	-	-	WL = 0.536(BP_a) + 51.277	0.301	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
CH-8	1	-0.7217	-0.5998	-0.5998	WL = -0.7217(BP_a) + 99.476	0.5761	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.4778			WL = -0.4778(BP_a) + 91.133	0.577	May 21, 2010 0900	May 24, 2010 1500	
CH-9	1	-0.6086	-0.5941	-0.594	WL = -0.6086(BP_a) + 264.94	0.6491	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.5795			WL = -0.5795(BP_a) + 263.93	0.465	May 23, 2010 1500	May 24, 2010 1500	
CH-10	1	0.1204	-	-	WL = 0.1204(BP_a) + 109.37	0.0895	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
	2	-0.6720	-	-	WL = -0.6724(BP_a) + 136.51	0.3470	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
CH-11	1	0.0270	-	-	WL =0.027(BP_a) + 69.492	0.0027	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	2	-0.6202	-	-	WL =-0.6202(BP_a) + 91.656	0.5361	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
CH-12	1	-0.5620	-	-0.5620	WL = -0.5623(BP_a) + 208.75	0.5168	May 23, 2010 1500	May 24, 2010 1500	
	2	0.5330	-	-	WL = 0.5335(BP_a) + 171.2	0.318	May 21, 2010 0900	May 24, 2010 1500	
CH-13	1	-0.6820	-	-0.682	WL = -0.6828(BP_a) + 230.8	0.5406	May 23, 2010 1500	May 24, 2010 1500	
	2	0.3690	-	-	WL = 0.3696(BP_a) + 194.74	0.174	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
CH-14	1	0.4301	-	-	WL = 0.4301(BP_a) + 214.8	0.2408	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	2	-0.4610	-	-	WL =-0.4618(BP_a) + 245.35	0.2568	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
CH-15	1	-0.5070	-0.6077	-0.608	WL = -0.507(BP_a) + 98.875	0.6263	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.7083			WL = -0.7083(BP_a) + 105.76	0.6244	May 23, 2010 1500	May 24, 2010 1500	
CH-17	1	-0.4202	-	-0.4202	WL = -0.4202(BP_a) + 265.47	0.2180	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.3281			WL = -0.3281(BP_a) + 262.32	0.2879	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
CH-18	1	-0.5589	-	-0.5589	WL = -0.5589(BP_a) + 177.14	0.4594	May 23, 2010 1500	May 24, 2010 1500	
	2	0.2919	-	-	WL =0.2919(BP_a) + 147.99	0.1539	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
CH-19	1	0.0210	-	-	WL = 0.021(BP_a) + 205.19	0.0049	May 21, 2010 0900	May 23, 2010 0200	Positive slope; BE not applicable
	2	-0.2202			WL = -0.2202(BP_a) + 213.42	0.1877	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
	3	-0.2511	-	-	WL = -0.2511(BP_a) + 214.47	0.1192	May 23, 2010 0300	May 24, 2010 1500	Low correlation; discard
CH-20	1	0.6177	-	-	WL = 0.6177(BP_a) + 118.07	0.6113	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
	2	1.6090	-	-	WL = 1.6097(BP_a) + 84.071	0.795	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
PW-37-XD-2	1	0.4309	-	-	WL = 0.4309(BP_a) + 166.9	0.2385	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(78.7 - 88.7)	2	-0.5975	-	-0.597	WL = -0.5975(BP_a) + 202.13	0.6371	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-3	1	-0.1157	-	-	WL = -0.1157(BP_a) + 242.82	0.4376	5/21/2010 1400	5/24/2010 1400	Discard - Poor Correlation
(90.7 - 100.7)	2	-0.0473	-	-	WL = -0.0473(BP_a) + 240.48	0.0533	5/23/2010 1400	5/24/10 2:00 PM	Discard - Poor Correlation
PW-37-XD-4	1	0.0292	-	-	WL = 0.0292(BP_a) + 182.97	0.0036	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(113.7 - 124.7)	2	-0.6753	-	-0.6753	WL = -0.6753(BP_a) + 207.09	0.8082	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-5	1	0.2857	-	-	WL = 0.2857(BP_a) + 176.04	0.1510	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(136.7 - 147.7)	2	-0.6843	-	-0.684	WL = -0.6843(BP_a) + 209.26	0.6479	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-6	1	0.2511	NA	NA	WL = 0.2511(BP_a) + 177.14	0.1238	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(195.7 - 205.7)	2	-0.6814	-0.681	-0.681	WL = -0.6814(BP_a) + 209.08	0.7118	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-7	1	0.2303	-	-	WL = 0.2303(BP_a) + 179.1	0.1217	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(208.7 - 218.7)	2	-0.6056	-	-0.6056	WL = -0.6056(BP_a) + 207.74	0.5588	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-8	1	0.2869	-	-	WL = 0.2869(BP_a) + 178.46	0.1342	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(245.7 - 256.7)	2	-0.7304	-	-0.7304	WL = -0.7304(BP_a) + 213.31	0.616	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-9	1	-0.0238	-	-	WL = -0.0238(BP_a) + 189.89	0.0013	5/21/10 11:00 AM	5/24/10 2:00 PM	Discard - Poor Correlation
(277.7 - 297.7)	2	-0.8086	-	-0.8086	WL = -0.8086(BP_a) + 216.77	0.5611	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-10	1	0.2684	-	-	WL = 0.2684(BP_a) + 181.42	0.0769	5/21/10 11:00 AM	5/24/10 2:00 PM	Positive BE, discard
(327.7 - 342.7)	2	-0.8951	-	-0.895	WL = -0.8951(BP_a) + 221.28	0.5244	5/23/10 2:00 PM	5/24/10 2:00 PM	
PW-37-XD-11	1	0.4391	-	-	WL = 0.4391(BP_a) + 177.2	0.1418	5/21/10 10:00 AM	5/24/10 2:00 PM	Positive BE, discard
(347.7 - 367.7)	2	-1.0316	-	-	WL = -1.0316(BP_a) + 227.59	0.5406	5/23/10 2:00 PM	5/24/10 2:00 PM	Barometric Efficiency >1.0 Discard
MW-1	1	-	-	-	WL = -0.9961(BP_a) + 43.043	0.6445	May 21, 2010 0900	May 24, 2010 1500	High BE; low correlation; discard
MW-2	1	-2.648	-	-	WL = -2.6482(BP_a) + 113.32	0.6161	May 21, 2010 0900	May 24, 2010 1500	BE > 1; discard
	2	-2.010	-	-	WL = -2.0101(BP_a) + 91.342	0.7721	May 23, 2010 1500	May 24, 2010 1500	BE > 1; discard
MW-3	1	-0.7701	-0.7884	-0.788	WL = -0.7701(BP_a) + 52.578	0.7301	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.8067			WL = -0.8067(BP_a) + 53.806	0.8172	May 23, 2010 1500	May 24, 2010 1500	
MW-5	1	-0.4461	-0.4089	-0.409	WL = -0.4461(BP_a) + 36.025	0.6426	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.3716			WL = -0.3716(BP_a) + 33.454	0.6753	May 23, 2010 1500	May 24, 2010 1500	
MW-6A	1	-0.3307	-	-0.331	WL = -0.3307(BP_a) + 22.975	0.6104	May 21, 2010 0900	May 24, 2010 1500	
	2	0.1557	-	-	WL = 0.1557(BP_a) + 6.2827	0.0559	May 23, 2010 1500	May 24, 2010 1500	Positive BE, discard
	3	-0.4024	-	-	WL = 0.1557(BP_a) + 6.2828	0.4505	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
MW-7A	1	-0.6902	-	-0.690	WL = -0.6871(BP_a) + 28.862	0.5162	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
MW-7C	1	-0.7986	-0.6962	-0.696	WL = -0.7986(BP_a) + 42.1	0.6799	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.5938			WL = -0.5938(BP_a) + 35.057	0.6902	May 23, 2010 1500	May 24, 2010 1500	

Table 8
Barometric Efficiency Summary Table

Well ID	Run	Barometric Efficiency	Ave. BE	BE Applied	Trend Equation[1]	R^2	Time Period		Comments
							Start	End	
MW-8A	1	-0.8333	-0.6323	-0.632	WL = -0.8333(BP_a) + 42.278	0.7229	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.4313			WL = -0.4313(BP_a) + 28.483	0.7264	May 23, 2010 1500	May 24, 2010 1500	
MW-10	1	-0.4699			WL = -0.4699(BP_a) + 21.75	0.7255	May 21, 2010 1500	May 23, 2010 1500	
	2	-0.1151	-0.366	-0.366	WL = -0.1151(BP_a) + 9.5784	0.5712	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.5130			WL = -0.513(BP_a) + 23.218	0.7204	May 21, 2010 0900	May 24, 2010 1500	
MW-12	1	0.0489	-	-	WL = 0.0489(BP_a) + 18.437	0.1021	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	2	-0.1659	-	-	WL =-0.1659(BP_a) + 25.796	0.3284	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
MW-15A	1	-	-	-	WL = -7.8796(BP_a) + 274.08	0.6903	May 21, 2010 0900	May 24, 2010 1500	High BE; low correlation; discard
MW-15B	1	-1.3806	-	-	WL = -1.3806(BP_a) + 60.834	0.667	May 21, 2010 0900	May 24, 2010 1500	BE > 1; discard
	2	-0.4340	-	-	WL = -0.434(BP_a) +28.37	0.4579	May 23,2010 1500	May 24, 2010 1500	
MW-18	1	-0.5543	-	-0.5543	WL = -0.5543(BP_a) + 26.442	0.7272	May 21, 2010 0900	May 24, 2010 1500	
MW-19A	1	-1.8338	-	-	WL = -1.8338(BP_a) + 67.855	0.6982	May 23, 2010 1500	May 24, 2010 1500	BE > 1; discard
	2	-3.4092	-	-	WL = -3.4092(BP_a) + 122.14	0.5637	May 21, 2010 1000	May 23, 2010 1400	BE > 1; discard
	3	-4.5788	-	-	WL = -4.5788(BP_a) + 162.04	0.6243	May 21, 2010 1000	May 24, 2010 1500	BE > 1; discard
MW-22A	1	-0.2832			WL = -0.2832(BP_a) + 42.694	0.7774	May 21, 2010 1500	May 23, 2010 1500	
	2	-0.3182	-0.3337	-0.334	WL = -0.3182(BP_a) + 43.867	0.8348	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.3998			WL = -0.3998(BP_a) + 46.674	0.7471	May 21, 2010 0900	May 24, 2010 1500	
MW-24	1	-0.4999	-0.5361	-0.536	WL = -0.4999(BP_a) + 29.541	0.5152	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.5722			WL = -0.5722(BP_a) + 31.99	0.7586	May 23, 2010 1500	May 24, 2010 1500	
MW-26A	1	1.6828	-	-	WL = 1.6828(BP_a) + 20.626	0.8422	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	2	1.2020			WL = 1.202(BP_a) - 4.1272	0.9334	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
MW-33		-0.4353	-	-0.435	WL = -0.4353(BP_a) + 25.266	0.6624	May 21, 2010 0900	May 24, 2010 1500	
MW-34	1	-0.8924	-0.9080	-0.908	WL = -0.8924(BP_a) + 42.909	0.7024	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.9236			WL = -0.9236(BP_a) + 43.943	0.785	May 23, 2010 1500	May 24, 2010 1500	
MW-35	1	-0.9931	-	-	WL = -0.9931(BP_a) + 46.589	0.7069	May 21, 2010 0900	May 24, 2010 1500	High BE; discard
	2	-0.9786	-	-	WL = -0.9786(BP_a) + 46.055	0.7922	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.6487	-	-	WL = -0.6487(BP_a) + 34.83	0.6958	May 21, 2010 0900	May 23, 2010 1400	
MW-36	1	-0.7575	-0.7585	-0.759	WL = -0.7575(BP_a) + 35.689	0.7476	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.7595			WL = -0.7595(BP_a) + 35.783	0.7156	May 21, 2010 0900	May 24, 2010 1500	
MW-37	1	-2.7512	-	-	WL = -2.7512(BP_a) + 107.26	0.6516	May 21, 2010 0900	May 24, 2010 1500	BE > 1; discard
	2	-1.5355	-	-	WL = -1.5355(BP_a) + 65.523	0.7545	May 23, 2010 1500	May 24, 2010 1500	BE > 1; discard
MW-38	1	-	-	-	WL = -0.009(BP_a) + 1.1361	0.1	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
MW-39A	1	-0.7358	-0.6346	-0.635	WL = -0.7358(BP_a) + 33.828	0.6915	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.5333			WL = -0.5333(BP_a) + 26.865	0.7201	May 23, 2010 1500	May 24, 2010 1500	
MW-40A	1	-0.6947	-0.6735	-0.673	WL = -0.6947(BP_a) + 51.705	0.7027	May 21, 2010 0900	May 24, 2010 1500	
	2	-0.6522			WL = -0.6522(BP_a) + 50.224	0.8234	May 23, 2010 1500	May 24, 2010 1500	
MW-41	1	-0.6280	-	-	WL = -0.628(BP_a) + 66.863	0.1086	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
	2	-1.1577	-	-	WL = -1.1577(BP_a) + 85.032	0.3862	May 21, 2010 0900	May 24, 2010 1500	
MW-42	1	-0.0849			WL = -0.0849(BP_a) + 8.8869	0.711	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.0554	-0.0828	-0.083	WL = -0.0554(BP_a) + 7.868	0.5431	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.1081			WL = -0.1081(BP_a) + 9.6763	0.7135	May 21, 2010 0900	May 24, 2010 1500	
MW-43	1	-0.2276			WL = -0.2276(BP_a) + 18.72	0.6367	May 21, 2010 1000	May 23, 2010 1400	
	2	-0.3056	-0.2313	-0.231	WL = -0.3056(BP_a) + 18.73	0.6714	May 21, 2010 1000	May 24, 2010 1500	
	3	-0.1607			WL = -0.1607(BP_a) + 16.408	0.6735	May 21, 2010 0900	May 24, 2010 1500	
MW-46	1	-0.4257	-	-0.426	WL = -0.4257(BP_a) + 23.066	0.9304	May 23, 2010 1500	May 24, 2010 1500	
	2	0.7226	-	-	WL =0.7226(BP_a) - 16.286	0.3647	May 21, 2010 0900	May 24, 2010 1500	Positive BE, discard
	3	-0.1246	-	-	WL =-0.1246(BP_a) + 12.743	0.0431	May 22, 2010 1500	May 24, 2010 1500	Low correlation; discard
MW-50	1	-0.2764	-0.3579	-0.358	WL = -0.2764(BP_a) + 42.181	0.5266	May 23, 2010 1400	May 24, 2010 1500	
	2	-0.4393			WL = -0.4393(BP_a) + 47.776	0.6655	May 21, 2010 0900	May 24, 2010 1500	
MW-52	1	-0.2204			WL = -0.2204(BP_a) + 23.864	0.6406	May 21, 2010 1000	May 23, 2010 1400	
	2	-0.3883	-0.3236	-0.324	WL = -0.3883(BP_a) + 29.585	0.7953	May 23, 2010 1400	May 24, 2010 1500	
	3	-0.3620			WL = -0.362(BP_a) + 28.696	0.6751	May 21, 2010 0900	May 24, 2010 1500	
MW-55	1	-0.6730	-	-	WL = -0.673(BP_a) + 35.074	0.1257	May 21, 2010 1000	May 24, 2010 1500	Low correlation; discard
	2	-0.0971			WL = -0.0971(BP_a) + 15.325	0.0019	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
MW-57	1	-0.3556			WL = -0.3556(BP_a) + 17.948	0.7164	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.2487	-0.3526	-0.353	WL = -0.2487(BP_a) + 14.26	0.7350	May 23, 2010 1400	May 24, 2010 1500	
	3	-0.4534			WL = -0.4534(BP_a) + 21.286	0.7284	May 21, 2010 0900	May 24, 2010 1500	
MW-59	1	-9.8969	-	-	WL = -9.8969(BP_a) + 348.51	0.6848	May 21, 2010 0900	May 24, 2010 1500	High BE; discard
	2	-2.9485			WL = -2.9485(BP_a) + 110.27	0.6831	May 23, 2010 1500	May 24, 2010 1500	High BE; discard
MW-60	1	-0.8085	-	-0.8085	WL = -0.8085(BP_a) + 34.404	0.8048	May 21, 2010 0900	May 24, 2010 1500	
MW-61	1	-0.0133	-	-	WL = -0.0133(BP_a) + 9.7746	0.0258	May 21, 2010 0900	May 23, 2010 1400	Low correlation; discard
	2	-0.1525	-	-	WL = -0.1525(BP_a) + 14.522	0.6472	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.1058	-	-	WL = -0.1058(BP_a) + 12.931	0.3368	May 21, 2010 0900	May 24, 2010 1500	
MW-63	1	-0.3163			WL = -0.3163(BP_a) + 42.107	0.7017	May 21, 2010 1500	May 23, 2010 1400	
	2	-0.4220	-0.3939	-0.394	WL = -0.4220(BP_a) + 45.696	0.5908	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.4434			WL = -0.4434(BP_a) + 46.443	0.7117	May 21, 2010 0900	May 24, 2010 1500	
MW-69	1	-0.5010			WL = -0.501(0BP_a) + 24.125	0.6018	May 21, 2010 0900	May 24, 2010 1500	
MW-70-1	1	-0.1798	-	-	WL = -0.1798(BP_a) + 33.943	0.4328	May 21, 2010 0900	May 23, 2010 1400	Low correlation; discard
	2	-0.3722			WL = -0.3722(BP_a) + 40.499	0.2743	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
	3	-0.3339			WL = -0.3339(BP_a) + 39.203	0.4762	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
MW-72	1	-	-	-	WL = -1.772(BP_a) + 68.465	0.7402	May 21, 2010 0900	May 24, 2010 1500	High BE; discard
MW-73	1	-0.5286	-0.5286	-0.5286	WL = -0.5286(BP_a) + 28.318	0.688	May 21, 2010 0900	May 24, 2010 1500	

Table 8
Barometric Efficiency Summary Table

Well ID	Run	Barometric Efficiency	Ave. BE	BE Applied	Trend Equation[1]	R^2	Time Period Start	Time Period End	Comments
MW-74	1	-0.2749	-0.3715	-0.372	WL = -0.2749(BP_a) + 37.572	0.7334	May 21, 2010 0900	May 24, 2010 1400	
	2	-0.4491			WL = -0.4491(BP_a) + 43.514	0.8347	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.3906			WL = -0.3906(BP_a) + 41.521	0.762	May 21, 2010 0900	May 24, 2010 1500	
MW-80	1	-0.8548	-0.8548	-0.8548	WL = -0.8548(BP_a) + 31.89	0.852	May 21, 2010 0900	May 24, 2010 1500	
MW-81	1	-	-	-	WL = -1.7831(BP_a) + 65.972	0.7286	May 21, 2010 0900	May 24, 2010 1500	High BE; discard
MW-103A	1	-	-	-	WL = -0.112(BP_a) + 10.57	0.2459	May 21, 2010 0900	May 24, 2010 1500	Low correlation; discard
MW-103B	1	-0.3526	-0.3872	-0.387	WL = -0.3526(BP_a) + 44.928	0.6477	May 21, 2010 1200	May 23, 2010 1400	
	2	-0.3244			WL = -0.3244(BP_a) + 43.931	0.6209	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.4847			WL = -0.4847(BP_a) + 49.437	0.6756	May 24, 2010 1200	May 23, 2010 1500	
MW-104A	1	-0.3661	-0.3661	-0.3661	WL = -0.3661(BP_a) + 18.847	0.7334	May 21, 2010 0900	May 24, 2010 1400	
MW-104B	1	1.0843	-	-	WL = 1.0843(BP_a) - 9.8875	0.8916	May 21, 2010 0900	May 24, 2010 1400	Positive slope; BE not applicable
	2	0.8006	-	-	WL = 0.8006(BP_a) - 0.1678	0.9005	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
MW-105B	1	-0.3528	-0.4063	-0.406	WL = -0.3528(BP_a) + 46.291	0.6331	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.3621			WL = -0.3621(BP_a) + 46.574	0.6900	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.5040			WL = -0.504(BP_a) + 51.451	0.6782	May 21, 2010 0900	May 24, 2010 1400	
MW-106A	1	-0.4770	-	-0.477	WL = -0.4772(BP_a) + 21.341	0.7334	May 21, 2010 0900	May 24, 2010 1400	
MW-106B	1	0.6847	-	-	WL = 0.6847(BP_a) + 3.997	0.8169	May 21, 2010 0900	May 23, 2010 1400	Positive slope; BE not applicable
	2	0.2116	-	-	WL = 0.2116(BP_a) + 20.192	0.0273	May 23, 2010 1500	May 24, 2010 1500	Positive slope; BE not applicable
	3	0.5757	-	-	WL = 0.5757(BP_a) + 7.7232	0.524	May 21, 2010 0900	May 24, 2010 1500	Positive slope; BE not applicable
	4	-0.0431	-	-	WL = -0.0431(BP_a) + 28.923	0.0007	May 24, 2010 0300	May 24, 2010 1500	
MW-107	1	-0.6953	-	-0.6953	WL = -0.6953(BP_a) + 47.671	0.7026	May 23, 2010 1500	May 24, 2010 1500	
	2	-2.1164	-	-	WL = -2.1164(BP_a) + 96.47	0.6442	May 21, 2010 0900	May 23, 2010 1400	BE > 1; discard
	3	-2.4693	-	-	WL = -2.4693(BP_a) + 108.50	0.6792	May 21, 2010 0900	May 24, 2010 1500	BE > 1; discard
MW-108A		>1			Spike in WL at 5/27 18:51	-			
MW-108B	1	-0.8324	-0.8399	-0.840	WL = -0.8324(BP_a) + 54.281	0.7055	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.8474			WL = -0.8474(BP_a) + 54.788	0.7280	May 21, 2010 0900	May 24, 2010 1500	
	3	-0.2142	-	-	WL = -0.2142(BP_a) + 33.089	0.8284	May 23, 2010 1500	May 24, 2010 1500	Discard
MW-113	1	-0.4520	-0.5889	-0.589	WL = -0.452(BP_a) + 70.579	0.7205	May 21, 2010 099	May 23, 2010 1400	
	2	-0.6506			WL = -0.6506(BP_a) + 77.336	0.7461	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.6641			WL = -0.6641(BP_a) + 77.821	0.7241	May 21, 2010 0900	May 24, 2010 1500	
MW-114	1	-0.3601	-0.4630	-0.463	WL = -0.3601(BP_a) + 44.973	0.5242	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.4210			WL = -0.421(BP_a) + 47.001	0.7208	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.6079			WL = -0.6079(BP_a) + 53.431	0.5932	May 21, 2010 0900	May 24, 2010 1500	
MW-115	1	-0.7400	-0.6349	-0.635	WL = -0.7400(BP_a) + 67.984	0.5677	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.5297			WL = -0.5297(BP_a) + 60.698	0.714	May 23, 2010 1500	May 24, 2010 1500	
	3	-1.0580	-	-	WL = -1.0581(BP_a) + 78.839	0.6287	May 21, 2010 0900	May 24, 2010 1500	BE > 1; discard
MW-116	1	-0.5082	-0.5347	-0.535	WL = -0.5082(BP_a) + 78.501	0.6898	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.4339			WL = -0.4339(BP_a) + 75.917	0.8433	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.662			WL = -0.662(BP_a) + 83.748	0.7303	May 21,2010 0900	May 24, 2010 1500	
MW-117	1	-0.8051	-0.6967	-0.697	WL = -0.8051(BP_a) + 85.07	0.7349	May 21, 2010 0900	May 23, 2010 1400	
	2	-0.5882			WL = -0.5882(BP_a) + 77.581	0.7325	May 23, 2010 1500	May 24, 2010 1500	
	3	-1.0270	-	-	WL = -1.0270(BP_a) + 77.582	0.739	May 21, 2010 0900	May 23, 2010 1400	BE > 1; discard
MW-118	1	-0.1851	-0.1525	-0.152	WL = -0.1851(BP_a) + 30.912	0.8644	May 24, 2010 0300	May 24, 2010 1500	
	2	-0.1198			WL = -0.1198(BP_a) + 28.674	0.5397	May 23, 2010 1500	May 24, 2010 1500	
	3	0.8555	-	-	WL =0.8555(BP_a) - 4.7497	0.5584	May 21,2010 0900	May 24, 2010 1500	BE > 1; discard
MW-119	1	-0.9697	-0.6160	-	WL = -0.9697(BP_a) + 99.034	0.3389	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
	2	-0.3720		-	WL = -0.3720(BP_a) + 78.579	0.0882	May 21,2010 1400	May 24, 2010 1500	Low correlation; discard
	3	-0.5064		-	WL = -0.5064(BP_a) + 83.174	0.1797	May 21,2010 0900	May 24, 2010 1500	Low correlation; discard
MW-120	1	-0.5073	-0.5095	-0.510	WL = -0.5073(BP_a) + 46.141	0.9716	May 23, 2010 1500	May 24, 2010 1500	
	2	-0.5095			WL = -0.5095(BP_a) + 46.218	0.9802	May 24, 2010 0300	May 24, 2010 1500	
	3	0.5415	-	-	WL =0.5415(BP_a) + 10.21	0.3544	May 21,2010 0900	May 24, 2010 1500	BE > 1; discard
MW-121	1	-0.9050	-0.6290	-0.905	WL = -0.905(BP_a) + 90.059	0.6563	May 21, 2010 1200	May 24, 2010 1500	
	2	-0.3530			WL = -0.353(BP_a) + 71.062	0.4867	May 23, 2010 1500	May 24, 2010 1500	Low correlation; discard
	3	-1.1359	-	-	WL = -1.1359(BP_a) + 97.913	0.6625	May 21, 2010 1000	May 24, 2010 1500	BE > 1; discard
MW-122	1	0.561	-	-	WL = -.5607(BP_a) + 4.1205	0.3069	May 21, 2010 1200	May 24, 2010 1500	Positive BE, discard
	2	-0.477	-0.5030	-0.503	WL = -0.4772(BP_a) + 39.688	0.9224	May 23, 2010 1500	May 24, 2010 1500	
	3	-0.529			WL = -0.5293(BP_a) + 41.473	0.9653	May 24, 2010 0300	May 24, 2010 1500	

Table 10

Summary of Drawdown Data

TABLE 10 SUMMARY OF DRAWDOWN DATA

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16	Static Groundwater Elev.	Post 72 Hrs Pumping Groundwater Elev.	Maxmium Drawdown (ft)	Time to First Drawdown (min)	Comments
CH-1	8	650	Deep Bedrock	1446	100.58	99.77	0.81	181.75	
CH-2	8	650	Deep Bedrock	2521	106.01	105.39	0.62	181.75	
CH-3	8	450	Deep Bedrock	2618	111.43	111.03	0.40	-	No response to pumping
CH-4	8	503	Deep Bedrock	2012	102.94	102.18	0.76	111.75	
CH-5	8	400	Deep Bedrock	1310	99.55	98.82	0.73	101.5	
CH-6	8	500	Deep Bedrock	989	99.55	97.84	1.71	121.75	
CH-7	8	500	Deep Bedrock	279	96.77	84.66	12.11	0.83	
CH-8	8	500	Deep Bedrock	1569	103.20	102.59	0.61	191.75	
CH-9	8	425	Deep Bedrock	1560	100.45	99.88	0.57	231.75	
CH-10	8	~450	Deep Bedrock	1145	98.52	90.8	7.72	21.50	
CH-11	8	~450	Deep Bedrock	1218	99.08	91.84	7.24	21.75	
CH-12	8	~450	Deep Bedrock	885	97.58	85.78	11.80	2.25	
CH-13	8	~450	Deep Bedrock	541	97.31	82.30	15.01	1.72	
CH-14	8	~450	Deep Bedrock	478	97.00	85.04	11.96	2.17	
CH-15	8	~450	Deep Bedrock	873	97.40	94.03	3.37	31.75	
CH-16*	8	~450	Pumping Well	0	96.70	60.59	36.11	-	Pumping Well
CH-17	8	~450	Deep Bedrock	907	93.91	90.10	3.81	31.50	
CH-18	8	~450	Deep Bedrock	456	96.23	84.55	11.68	1.83	
CH-19	8	~450	Deep Bedrock	936	70.22	69.79	0.43	71.75	
CH-20	8	~450	Deep Bedrock	158	97.21	81.44	15.77	1.75	
MW-113 (CH-11)	6	80	Shallow Bedrock	1233	105.89	102.48	3.41	61.65	
MW-114 (CH-12)	6	80	Shallow Bedrock	904	112.95	112.17	0.78	101.75	
MW-115 (CH-13)	6	80	Shallow Bedrock	537	110.50	109.82	0.68	191	
MW-116 (CH-14)	6	80	Shallow Bedrock	456	107.71	106.3	1.41	201.75	
MW-117 (CH-15)	6	80	Shallow Bedrock	872	98.72	97.31	1.41	161.75	
MW-118 (CH-16)	6	80	Shallow Bedrock	20	96.85	86.06	10.79	101.50	
MW-119 (CH-17)	6	80	Shallow Bedrock	890	89.39	87.97	1.42	21.75	
MW-120 (CH-18)	6	80	Shallow Bedrock	441	96.66	89.88	6.78	151.50	
MW-121 (CH-19)	6	80	Shallow Bedrock	935	93.84	92.66	1.18	51.75	
MW-122 (CH-20)	6	80	Shallow Bedrock	166	95.79	85.00	10.79	61.75	
ML-37	10	728.5	Deep Bedrock	327	-	-	-	-	Multi-level sampling flute installed in well
MW-1	4	14.3	Overburden/Bedrock	2048	115.49	115.46	0.03	-	No clear response to pumping
MW-2	6	30.5	Shallow Bedrock	1592	115.20	114.59	0.61	71.50	
MW-3	6	79	Shallow Bedrock	674	110.44	109.1	1.34	211.50	
MW-5	6	30	Shallow Bedrock	1673	107.32	107.01	0.31	181.50	
MW-6A	4	25	Shallow Bedrock	1395	102.77	102.44	0.33	491.50	
MW-7A	2	15.5	Overburden	1029	96.89	96.55	0.34		
MW-7C	2	30	Shallow Bedrock	1147	98.88	98.30	0.58	171.75	
MW-8A	6	33	Shallow Bedrock	546	104.06	102.36	1.70	181.75	
MW-10	4	14.8	Overburden/Bedrock	575	111.70	111.52	0.18	531.50	
MW-12	6	50	Shallow Bedrock	412	126.58	126.53	0.05	-	No clear response to pumping

TABLE 10 SUMMARY OF DRAWDOWN DATA

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16	Static Groundwater Elev.	Post 72 Hrs Pumping Groundwater Elev.	Maxmium Drawdown (ft)	Time to First Drawdown (min)	Comments
MW-15A	2	15	Overburden	804	101.09	100.17	0.92	333.75	
MW-15B	3	30	Shallow Bedrock	804	100.26	99.38	0.88	191.50	
MW-18	4	19	Overburden	810	96.87	95.88	0.99	188.75	
MW-19A	4	18	Overburden/Bedrock	338	107.73	107.35	0.38	61.75	
MW-22A	3	45	Shallow Bedrock	1299	100.20	99.92	0.28	441.75	
MW-24	6	42	Shallow Bedrock	1262	111.08	110.46	0.62	201.75	
MW-26A	6	50.5	Shallow Bedrock	942	94.97	93.53	1.44	61.75	
MW-33	2	23	Overburden/Bedrock	965	93.21	91.06	2.15	41.50	
MW-34	2	49.3	Shallow Bedrock	580	110.69	109.20	1.49	211.75	
MW-35	2	49.9	Shallow Bedrock	497	108.85	107.70	1.15	295.50	
MW-36	2	49.7	Shallow Bedrock	347	108.77	107.24	1.53	111.75	
MW-37	6	34.9	Shallow Bedrock	692	115.14	114.75	0.39	41.50	
MW-38	2	6.5	Overburden	441	112.92	112.92	0.00	-	No response to pumping
MW-39A	2	18.5	Shallow Bedrock	436	110.86	110.29	0.57	211.75	
MW-39-1	4	21.5	Overburden/Bedrock	1435	NM	110.38	1.27	-	Manual depth to water measurements
MW-40A	2	39	Shallow Bedrock	433	109.59	108.77	0.82	181.75	
MW-41	2	58.7	Shallow Bedrock	436	107.26	105.02	2.24	91.75	
MW-42	2	17.2	Overburden/Bedrock	414	108.87	108.84	0.03	-	No clear response to pumping
MW-43	2	24.5	Shallow Bedrock	1958	111.53	111.36	0.17	181.5	
MW-46	6	62	Shallow Bedrock	512	95.13	90.07	5.06	231.75	
MW-50	6	45	Shallow Bedrock	1419	102.23	101.89	0.34	161.5	
MW-52	6	30	Shallow Bedrock	1444	102.64	102.38	0.26	201.75	
MW-55	6	26	Shallow Bedrock	972	92.32	89.69	2.63	111.75	
MW-57	6	17.5	Shallow Bedrock	1116	89.92	87.04	2.88	121.75	
MW-58	2	36.7	Shallow Bedrock	2349	119.91	119.82	0.09	-	Manual depth to water measurements
MW-59	6	25.5	Shallow Bedrock	1774	113.58	113.08	0.50	21.5	
MW-60	2	22	Overburden/Bedrock	1362	112.03	111.81	0.22	-	No clear response to pumping
MW-61	6	41	Shallow Bedrock	1106	129.46	129.45	0.01	-	No clear response to pumping
MW-63	2	41.5	Shallow Bedrock	892	93.97	90.93	3.04	31.75	
MW-69	4	18.2	Overburden/Bedrock	992	93.02	92.54	0.48	198	
MW-70-1	6	35.4	Shallow Bedrock	1718	106.05	106.00	0.05	-	No clear response to pumping
MW-72	4	20	Overburden	968	92.88	92.00	0.88	238	
MW-73	4	22	Overburden/Bedrock	958	92.00	89.84	2.16	33.75	
MW-74	6	40	Shallow Bedrock	968	93.26	90.81	2.45	71.75	
MW-80	2	18.5	Overburden/Bedrock	1295	111.02	110.88	0.14	-	No clear response to pumping
MW-81	2	20	Overburden	917	106.10	105.43	0.67	-	No clear response to pumping
MW-103A	2	15	Overburden/Bedrock	1165	93.72	93.62	0.10	-	No clear response to pumping
MW-103B	6	37.4	Shallow Bedrock	1162	96.82	96.30	0.52	50	
MW-104A	2	13.3	Overburden/Bedrock	1097	91.04	90.69	0.35	65	
MW-104B	6	33.7	Shallow Bedrock	1096	92.34	90.98	1.36	20	
MW-105B	6	38.7	Shallow Bedrock	1380	97.30	96.83	0.47	40	

TABLE 10 SUMMARY OF DRAWDOWN DATA

Well ID #	Well Diameter (in)	Well Depth (ft bgs)	Well Type	Distance from CH-16	Static Groundwater Elev.	Post 72 Hrs Pumping Groundwater Elev.	Maxmium Drawdown (ft)	Time to First Drawdown (min)	Comments
MW-106A	2	12.3	Overburden/Bedrock	1088	90.52	89.87	0.65	60	
MW-106B	6	33.8	Shallow Bedrock	1090	93.08	92.41	0.67	500	
MW-107	6	32	Shallow Bedrock	1199	91.62	90.3	1.32	90	
MW-108A	2	10.7	Overburden	1274	89.15	88.85	0.30	-	No clear response to pumping
MW-108B	6	31.8	Shallow Bedrock	1274	91.77	90.19	1.58	40	

Notes:

1. CH-16 is the pumping well. A well efficiency of 21.6% was used to calculate maximum drawdown
2. All elevations are NAVD 1988, feet
3. Static groundwater elevations are from 5/24/10 at 1530.
4. Maximum drawdown at MW-39-1 calculated from an initial elevation measured 1 hour after the start of the pump test.

Table 11

Summary of Aquifer Test Analytical Methods/Model Assumption

Table 11. Summary of Aquifer Test Analytical Methods/Models Assumptions.

Method	Aquifer	Aquifer is of infinite areal extent	Aquifer is homogenous and isotropic	Flow is unsteady	Aquifer potentiometric surface is initially horizontal	Pumping well screen	Characteristics
Neuman Witherspoon (1969)	leaky confined	x	x	x	x	Fully penetrating	Accounts for drawdown in the unpumped aquifer.
Hantush and Jacob (1955)	leaky confined	x	x	x		Fully or partially penetrating	No drawdown in the unpumped aquifer.
Hantush (1960)	leaky confined	x	x	x		Fully or partially penetrating	No drawdown in the unpumped aquifer.
Moench (1985), case 1	leaky confined	x	x	x	x	Fully penetrating	Aquitard overlain/underlain by constant head boundary.
Moench (1985)[1], case 2	leaky confined	x	x	x	x	Fully penetrating	Aquitard overlain/underlain by a no flow boundary.
Cooper-Jacobs (1946)	confined	x	x	x		Fully penetrating	
Papadopulos-Cooper (1967)	confined	x	x	x		Fully penetrating	
Theis (1935)[1]	confined	x	x	x		Fully penetrating	

Notes:

[1] Recovery Analysis Only

Table 12

Summary of Aquifer Characterization Determination
by Pump Test Data Analyses

TABLE 12 SUMMARY OF AQUIFER CHARACTERISTICS DETERMINED BY PUMP TEST DATA ANALYSIS

	Barometric Efficiency	Trend Equation[1]	R^2	BP Correction Applied? (Y/N)	Transmissivity (ft^2/min)								Storativity							
					Leaky - Hantush-Jacob - no storage	*Leaky - Hantush-Jacob - storage*	*Leaky - Moench (Case 1)*	*Leaky - Moench (Case 2)*	*Leaky - Neuman Witherspoon*	*Confined - Thesis*	*Confined - Papadopulos-Cooper*	*Confined - Cooper-Jacobs*	*Leaky - Hantush-Jacob - no storage*	*Leaky - Hantush-Jacob - storage*	*Leaky - Moench (Case 1)*	*Leaky - Moench (Case 2)*	*Leaky - Neuman Witherspoon*	*Confined - Thesis*	*Confined - Papadopulos-Cooper*	*Confined - Cooper-Jacobs*
CH-16	0	-	-																	
CH-7	51.6%	WL = -0.516(BP_a) + 87.316	0.5277	Y	7.95E-01	5.04E-01	4.25E-01	3.47E-01	4.17E-01	8.35E-01	**8.49E-01**	3.98E-01	7.22E-04	2.94E-05	5.55E-04	5.86E-04	2.45E-05	1.82E-04	**7.09E-04**	2.29E-03
CH-13	68.2%	WL = -0.6828(BP_a) + 230.8	0.5406	Y	5.52E-01	5.74E-01	4.88E-01	7.70E-01	1.68E-01	7.62E-01	7.75E-01	3.70E-01	1.32E-04	1.01E-04	1.14E-04	8.84E-05	3.73E-06	9.86E-05	9.26E-05	3.68E-04
CH-14	-	WL = 0.4301(BP_a) + 214.8	0.2408	N	4.57E-01	8.37E-01	4.43E-01	1.00E+00	8.40E-01	1.14E+00	1.17E+00	4.05E-01	2.93E-04	8.55E-05	2.54E-04	1.57E-04	8.54E-05	5.80E-05	5.15E-05	7.72E-04
CH-18	55.8%	WL = -0.5589(BP_a) + 177.14	0.4594	Y	7.02E-01	7.02E-01	6.29E-01	8.61E-01	7.02E-01	9.33E-01	9.39E-01	5.08E-01	2.38E-04	1.95E-04	2.13E-04	2.33E-04	1.95E-04	2.01E-04	1.95E-04	5.85E-04
CH-20	-	WL = 0.6177(BP_a) + 118.07	0.6177	N	5.12E-01	8.65E-01	failed	failed	8.65E-01	7.51E-01	1.28E+00	3.81E-01	8.03E-04	1.44E-04	failed	failed	1.44E-04	1.41E-04	9.08E-05	3.15E-03
PW-37																				
MW-1	100%	WL = -0.9961(BP_a) + 43.043	0.6445	N	Drawdown doesn't seem to be due to pumping at PW															
MW-115	63.5% (Ave.)	WL = -0.74(BP_a) + 67.984	0.5677	N	Skipped - low drawdown															
		WL = -0.5297(BP_a) + 60.698	0.714																	
MW-116	53.8%	WL = -0.5082(BP_a) + 78.501	0.6898	Y	2.75E+00	8.84E-01	2.09E+00	1.97E+00	2.47E+00	2.31E+00	2.23E+00	1.62E+00	1.56E-02	2.83E-02	1.59E-02	2.18E-02	2.15E-02	2.21E-02	1.83E-02	1.86E-02
		WL = -0.4339(BP_a) + 75.917	0.8433																	
		WL = -0.4339(BP_a) + 75.917	0.7303																	
MW-118	15.2%	WL = -0.1851(BP_a) + 30.912	0.8644	Y	3.35E-01	4.80E-01	5.32E-02	6.13E-01	Failed	6.54E-01	Poor	3.25E-01	7.39E-01	2.13E-01	8.62E-02	7.70E-02	Failed	1.00E-01	Poor	7.83E-01
		WL = -0.1198(BP_a) + 28.674	0.5397																	
MW-120	50.7%	WL = -0.5073(BP_a) + 46.141	0.9716	Y	6.70E-02	4.27E-01	7.81E-03	4.25E-01	4.27E-01	6.01E-01	6.03E-01	3.39E-01	1.17E-03	1.18E-03	1.43E-04	1.10E-03	1.18E-03	1.44E-03	1.43E-03	1.78E-03
MW-122	50.3%	WL = -0.4772(BP_a) + 39.687	0.9224	Y	3.40E-01	4.29E-01	2.53E-01	0.5273	4.29E-01	6.04E-01	6.07E-01	4.16E-01	8.17E-03	5.84E-03	5.89E-03	0.00627	5.84E-03	7.09E-03	7.00E-03	8.48E-03
		WL = -0.5293(BP_a) + 41.473	0.9653																	
MW-12	-	WL = 0.0716(BP_a) + 17.66	0.3284	N	Skipped - low drawdown															
MW-38	-	WL = -0.009(BP_a) + 1.1361	0.1	N	No response to pumping															
MW-39A	63.4%	WL = -0.7358(BP_a) + 33.828	0.6915	Y	4.64E+00	5.52E+00	4.20E+00	4.31E+00	3.95E+00	4.14E+00	4.46E+00	2.93E+00	7.18E-02	7.79E-02	5.50E-02	6.07E-02	5.71E-02	5.28E-02	5.44E-02	3.85E-02
		WL = -0.5333(BP_a) + 26.865	0.7201																	
MW-40A	67.3%	WL = -0.6947(BP_a) + 51.705	0.7027	Y	3.69E+00	3.56E+00	3.51E+00	2.48E+00	Poor	3.82E+00	2.33E+00	2.33E+00	4.08E-02	4.27E-02	3.74E-02	3.78E-02	Poor	3.89E-02	3.15E-02	3.15E-02
		WL = -0.6522(BP_a) + 50.224	0.8234																	
MW-41	62.8%	WL = -0.628(BP_a) + 66.863	0.1086	Y	Failed	Poor	Poor	Poor	Poor	Poor	Poor	1.08E+00	Failed	Poor	Poor	Poor	Poor	Poor	Poor	1.02E-02
MW-34	90.8%	WL = -0.8924(BP_a) + 42.909	0.7024	Y	1.57E+00	2.20E+00	1.97E+00	1.07E+00	Poor	1.01E+00	failed	1.62E+00	1.22E-02	1.22E-02	1.10E-02	1.13E-02	Poor	9.77E-03	failed	1.11E-02
		WL = -0.9236(BP_a) + 43.943	0.785																	
MW-35	100.0%	WL = -0.9931(BP_a) + 46.589	0.7069	N	3.94E-01	2.14E+00	1.65E+00	2.35E+00	1.39E+00	2.38E+00	1.41E+00	3.76E+00	7.05E-03	2.33E-02	1.98E-02	2.20E-02	5.75E-04	1.97E-02	2.91E-02	1.94E-02
MW-36	75.8%	WL = -0.7575(BP_a) + 35.689	0.7476	Y	2.61E+00	2.95E+00	2.21E+00	2.95E+00	2.56E+00	2.79E+00	2.51E+00	1.38E+00	1.75E-02	2.04E-02	4.05E-02	1.91E-02	1.66E-02	2.46E-02	2.25E-02	2.85E-02
MW-46	42.5%	WL = -0.4257(BP_a) + 23.066	0.9304	Y	3.69E-01	3.99E-01	3.47E-01	5.84E-01	6.02E-01	5.81E-01	5.81E-01	4.29E-01	4.60E-03	3.57E-03	4.29E-03	4.52E-03	4.31E-03	4.67E-03	4.66E-03	3.77E-03
MW-10	36.6% (Ave.)	WL = -0.4699(BP_a) + 21.75	0.7255	Y	Drawdown doesn't seem to be due to pumping at PW															
		WL = -0.1151(BP_a) + 9.5784	0.5712																	
		WL = -0.513(BP_a) + 23.218	0.7204																	
MW-42	8.2% (Ave.)	WL = -0.0849(BP_a) + 8.8869	0.711	Y	Little to no drawdown; 0.05 ft															
		WL = -0.0554(BP_a) + 7.868	0.5431																	
		WL = -0.1081(BP_a) + 9.6763	0.7135																	
MW-19A	Drawdown doesn't seem to be due to pumping at PW			N	Poor	1.47E+01	Poor	Poor	Poor	1.31E+01	1.54E+01		Poor	4.02E-02	Poor	Poor	Poor	4.67E-02	4.36E-02	

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TABLE 12 SUMMARY OF AQUIFER CHARACTERISTICS DETERMINED BY PUMP TEST DATA ANALYSIS

	Barometric Efficiency	Trend Equation[1]	R^2	BP Correction Applied? (Y/N)	Transmissivity (ft^2/min): Leaky-Hantush-Jacob - no storage	Leaky-Hantush-Jacob - storage	Leaky - Moench (Case 1)	Leaky - Moench (Case 2)	Leaky - Neuman Witherspoon	Confined - Thesis	Confined - Papadopulos-Cooper	Confined - Cooper-Jacobs	Storativity: Leaky-Hantush-Jacob - no storage	Leaky-Hantush-Jacob - storage	Leaky - Moench (Case 1)	Leaky - Moench (Case 2)	Leaky - Neuman Witherspoon	Confined - Thesis	Confined - Papadopulos-Cooper	Confined - Cooper-Jacobs
CH-16	0	-	-																	
CH-2	85% (Ave)	WL = -0.6994(BP_a) + 99.149	0.7389	Y	5.66E+00	4.56E+00	3.36E+00	4.59E+00	failed	6.03E+00	5.27E+00	2.45E+00	1.72E-03	1.21E-03	1.48E-03	1.18E-03	failed	1.20E-03	1.55E-03	1.10E-03
		WL = -0.9065(BP_a) + 106.18	0.6805																	
		WL = -0.9597(BP_a) + 108.04	0.741																	
CH-3	15.0%	WL = .1502(BP_a) + 71.248	0.1409	N	Not Analyzed; doesn't seem to be responding to pump test; Aqtesolv file created															
CH-4	83% (Ave)	WL = -0.8614(BP_a) + 104.35	0.7153	Y	4.47E+00	5.02E+00	6.70E+00	4.67E+00	3.49E+00	3.41E+00	3.37E+00	2.53E+00	1.21E-03	1.56E-03	1.84E-03	1.47E-03	1.34E-03	1.40E-03	1.36E-03	1.46E-03
		WL = -0.8028(BP_a) + 102.36	0.7067																	
CH-6	71.9%	WL = -0.7885(BP_a) + 101.13	0.8727																	
		WL = -0.6503(BP_a) + 96.411	0.7838	Y	2.09E+00	1.88E+00	1.88E+00	1.87E+00	Poor	1.87E+00	2.61E+00	1.69E+00	2.90E-03	3.01E-03	3.02E-03	3.02E-03	Poor	3.03E-03	2.47E-03	2.49E-03
CH-8	59.9% (Ave.)	WL = -0.7217(BP_a) + 99.476	0.5761																	
		WL = -0.4778(BP_a) + 91.133	0.577	Y	3.96E+00	3.86E+00	4.07E+00	3.75E+00	5.25E+00	3.85E+00	3.81E+00	3.76E+00	4.91E-03	4.97E-03	5.00E-03	5.09E-03	2.78E-03	4.98E-03	5.00E-03	2.92E-03
CH-10	12.0%	WL = 0.1204(BP_a) + 109.37	0.0895	N	6.56E-01	1.04E+00	7.95E-01	1.02E+00	Poor	1.09E+00	9.63E-01	7.18E-02	1.45E-04	1.34E-04	1.35E-04	1.28E-04	Poor	1.37E-04	1.38E-04	1.67E-04
CH-11	53.6%	WL = -0.6202(BP_a) + 91.656	0.5361	N	6.40E-01	8.54E-01	5.68E-01	6.93E-01	6.78E-01	1.20E+00	9.40E-01	7.62E-01	1.37E-04	1.22E-04	1.44E-04	5.98E-05	1.59E-04	1.40E-04	1.10E-04	1.63E-04
CH-12	56.2%	WL = -0.5623(BP_a) + 208.75	0.5168	Y	5.98E-01	5.95E-01	3.25E-01	5.95E-01	5.95E-01	7.95E-01	8.00E-01	4.21E-01	1.05E-04	8.59E-05	5.41E-05	8.59E-05	8.59E-05	9.31E-05	1.70E-04	2.26E-04
MW-113	58.9%	WL = -0.452(BP_a) + 70.579	0.7205																	
		WL = -0.6506(BP_a) + 77.336	0.7461	Y	Poor	1.73E+00	Poor	1.44E+00	3.61E-02	1.94E+00	1.83E+00	1.18E+00	Poor	5.13E-04	Poor	5.50E-05	1.16E-06	5.89E-04	5.21E-04	6.18E-04
MW-114	46.3%	WL = -0.3601(BP_a) + 44.973	0.5242																	
		WL = -0.421(BP_a) + 47.001	0.7208	Y	Poor	3.86E-01	2.05E-01	5.29E-01	3.44E-02	5.29E+00	Poor	2.41E+00	Poor	3.47E-05	1.89E-05	3.76E-05	2.55E-05	4.67E-03	Poor	8.47E-03
		WL = -0.6079(BP_a) + 53.431	0.5932																	
MW-2	-	WL = -2.6482(BP_a) + 113.32	0.6161	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-3	78.8% (Ave.)	WL = -0.7701(BP_a) + 52.578	0.7301	Y	Not Analyzed; doesn't seem to be responding to pump test															
		WL = -0.8067(BP_a) + 53.806	0.8172																	
MW-24	53.6%	WL = -0.4999(BP_a) + 29.541	0.5152	Y	9.33E-01	3.16E+00	9.76E-01	2.99E+00	2.77E+00	2.64E+00	3.70E+00	3.47E+00	1.44E-03	5.04E-03	2.11E-03	4.51E-03	5.67E-03	5.40E-03	6.93E-03	5.00E-03
		WL = -0.5722(BP_a) + 31.99	0.7586																	
MW-37	-	WL = -2.7512(BP_a) + 107.26	0.6516	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-59	-	WL = -9.8969(BP_a) + 348.51	0.6848	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-60	80.8%	WL = -0.8085(BP_a) + 34.404	0.8048	Y	Not Analyzed; doesn't seem to be responding to pump test															
MW-61	-	WL = -0.0133(BP_a) + 9.7746	0.0258	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-80	85.5%	WL = -0.8548(BP_a) + 31.89	0.852	Y	Not Analyzed; doesn't seem to be responding to pump test															
MW-81	-	WL = -1.7831(BP_a) + 65.972	0.7286	N	Not Analyzed; doesn't seem to be responding to pump test															

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	Barometric Efficiency	Trend Equation[1]	R^2	BP Correction Applied? (Y/N)	Transmissivity (ft^2/min): Leaky-Hantush-Jacob - no storage	Leaky-Hantush-Jacob - storage	Leaky - Moench (Case 1)	Leaky - Moench (Case 2)	Leaky - Neuman Witherspoon	Confined - Thesis	Confined - Papadopulos-Cooper	Confined - Cooper-Jacobs	Storativity: Leaky-Hantush-Jacob - no storage	Leaky-Hantush-Jacob - storage	Leaky - Moench (Case 1)	Leaky - Moench (Case 2)	Leaky - Neuman Witherspoon	Confined - Thesis	Confined - Papadopulos-Cooper	Confined - Cooper-Jacobs
CH-16	0	-	-																	
CH-1	-	$WL = 0.4408(BP_a) + 67.818$	0.7239	N	Poor	5.18E+00	5.44E-02	4.32E+00	Poor	9.09E+00	1.08E+01	2.24E+00	Poor	1.21E-03	6.82E-05	3.22E-03	Poor	1.83E-03	7.63E-04	2.60E-03
CH-15	60.8%	$WL = -0.507(BP_a) + 98.875$	0.6263	Y	2.03E+00	1.26E+00	1.26E+00	1.28E+00	1.28E+00	2.04E+00	2.04E+00	1.33E+00	7.38E-04	5.32E-04	5.35E-04	5.30E-04	5.29E-04	7.38E-04	7.35E-04	1.02E-03
		$WL = -0.7083(BP_a) + 105.76$	0.6244																	
CH-17	42.0%	$WL = -0.4202(BP_a) + 265.47$	0.2180	Y	1.59E+00	?	1.35E+00	1.53E+00	4.13E-01	1.76E+00	2.04E+00	1.13E+00	4.95E-04	?	4.29E-04	3.91E-04	7.67E-05	6.00E-04	4.59E-04	8.43E-04
MW-117	69.7%	$WL = -0.8051(BP_a) + 85.07$	0.7349	Y	2.19E+00	2.14E+00	2.03E+00	2.03E+00	2.14E+00	2.14E+00	2.05E+00	2.03E+00	5.53E-03	5.62E-03	5.94E-03	5.96E-03	5.62E-03	5.63E-03	5.96E-03	3.94E-03
		$WL = -0.5882(BP_a) + 77.581$	0.7325																	
MW-119	-	$WL = -0.9697(BP_a) + 99.034$	0.3389	N	1.59E+00	1.56E+00	1.45E+00	1.88E+00	1.93E+00	1.88E+00	1.88E+00	1.57E+00	4.94E-04	4.08E-04	3.92E-04	5.65E-04	4.57E-04	4.62E-04	5.65E-04	6.99E-04
MW-5	40.9% (Ave.)	$WL = -0.4461(BP_a) + 36.025$	0.6426	Y	Not Analyzed; doesn't seem to be responding to pump test															
		$WL = -0.3716(BP_a) + 33.454$	0.6753																	
MW-6A	33.0%	$WL = -0.3307(BP_a) + 22.975$	0.6104	Y	Not Analyzed; doesn't seem to be responding to pump test															
MW-7A	69.0%	$WL = -0.6902(BP_a) + 28.976$	0.7179	Y	Not Analyzed; doesn't seem to be responding to pump test															
MW-7C	69.6% (Ave.)	$WL = -0.7986(BP_a) + 42.1$	0.6799	Y	4.25E+00	4.75E+00	2.88E+00	4.17E+00	3.16E+00	9.19E+00	5.89E+00	3.35E+00	7.66E-03	5.77E-03	1.15E-02	5.23E-03	1.05E-02	3.53E-03	3.92E-03	5.69E-03
		$WL = -0.5938(BP_a) + 35.057$	0.6902																	
MW-8A	63.2%	$WL = -0.8333(BP_a) + 42.278$	0.7229	Y	2.10E+00	2.04E+00	1.75E+00	2.07E+00	1.53E+00	1.77E+00	1.89E+00	1.24E+00	6.19E-03	6.68E-03	9.08E-03	7.13E-03	8.30E-03	1.10E-02	9.34E-03	1.04E-02
		$WL = -0.4313(BP_a) + 28.483$	0.7264																	
MW-15A	-	$WL = -7.8796(BP_a) + 274.08$	0.6903	N	2.48E+00	2.07E+00	2.37E+00	2.42E+00	2.26E+00	1.17E+00	2.33E+00	1.31E+00	9.73E-03	1.00E-02	9.49E-03	8.86E-03	9.71E-03	1.33E-02	9.90E-03	9.25E-03
MW-15B	-	$WL = -1.3806(BP_a) + 60.834$	0.667	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-18	55.4%	$WL = -0.5543(BP_a) + 26.442$	0.7272	Y	1.85E+00	1.80E+00	2.60E+00	1.83E+00	2.71E+00	2.07E+00	1.88E+00	2.13E+00	6.04E-03	5.51E-03	6.57E-03	7.06E-03	6.61E-03	6.39E-03	6.13E-03	5.91E-03
MW-22A	33.3%	$WL = -0.2832(BP_a) + 42.694$	0.7774	Y	4.51E+00	4.48E+00	4.10E+00	4.44E+00	4.47E+00	4.48E+00	4.46E+00	4.33E+00	1.84E-02	1.84E-02	1.96E-02	1.85E-02	1.84E-02	1.84E-02	1.84E-02	1.08E-02
		$WL = -0.3182(BP_a) + 43.867$	0.8348																	
		$WL = -0.3998(BP_a) + 46.674$	0.7471																	
MW-26A	-	$WL = 1.6828(BP_a) + 20.626$	0.8422	N	7.99E-01	4.49E+00	1.12E+00	4.84E+00	4.61E+00	4.81E+00	4.97E+00	1.98E+00	1.25E-03	2.00E-03	1.01E-03	2.03E-03	1.30E-03	1.23E-03	1.93E-03	2.82E-03
MW-33	43.5%	$WL = -0.4353(BP_a) + 25.266$	0.6624	Y	2.20E+00	1.89E+00	1.80E+00	2.77E+00	1.58E+00	2.90E+00	2.85E+00	1.54E+00	8.48E-04	9.38E-04	9.88E-04	9.20E-04	5.77E-04	8.54E-04	8.98E-04	1.76E-03
MW-50	35.8%	$WL = -0.2764(BP_a) + 42.181$	0.5266	Y	1.32E+01	8.70E+00	1.69E+01	6.71E+00	3.99E-01	8.48E+00	1.16E+01	6.42E+00	5.47E-03	5.44E-03	7.45E-03	4.17E-03	9.58E-05	5.67E-03	6.61E-03	6.68E-03
		$WL = -0.4393(BP_a) + 47.776$	0.6655																	
MW-52	32.3%	$WL = -0.2204(BP_a) + 23.864$	0.6406	Y	9.83E+00	1.02E+01	7.39E+00	7.54E+00	7.47E+00	6.95E+00	8.26E+00	4.97E+00	1.24E-02	1.07E-02	9.60E-03	1.10E-02	1.15E-02	1.16E-02	1.20E-02	1.06E-02
		$WL = -0.3883(BP_a) + 29.585$	0.7953																	
		$WL = -0.362(BP_a) + 28.696$	0.6751																	
MW-63	39.4%	$WL = -0.3163(BP_a) + 42.107$	0.7017	Y	3.18E+00	2.29E+00	2.28E+00	2.28E+00	2.57E+00	2.29E+00	2.29E+00	1.42E+00	4.62E-04	7.42E-04	7.47E-04	7.47E-04	3.15E-04	7.41E-04	7.41E-04	1.19E-03
		$WL = -.422(BP_a) + 45.696$	0.5908																	
MW-69	50.1%	$WL = -0.501(BP_a) + 24.125$	0.6018	Y	4.15E+00	3.19E+00	3.19E+00	3.18E+00	3.19E+00	3.18E+00	3.26E+00	3.14E+00	9.48E-03	9.59E-03	9.59E-03	9.60E-03	9.59E-03	9.58E-03	9.81E-03	6.28E-03
MW-72	-	$WL = -1.772(BP_a) + 68.465$	0.7402	N	2.68E+00	2.59E+00	3.63E+00	2.79E+00	2.93E+00	4.02E+00	2.80E+00	3.24E+00	6.95E-03	6.56E-03	6.34E-03	7.03E-03	6.14E-03	5.81E-03	7.11E-03	5.82E-03
MW-73	52.8%	$WL = -0.5286(BP_a) + 28.318$	0.688	Y	2.17E+00	2.04E+00	2.03E+00	2.01E+00	2.01E+00	2.00E+00	1.77E+00	1.13E+00	1.52E-03	1.60E-03	1.60E-03	1.61E-03	1.61E-03	1.61E-03	1.96E-03	2.06E-03
MW-74	37.1%	$WL = -0.2749(BP_a) + 37.572$	0.7334	Y	2.17E+00	1.80E+00	1.80E+00	1.25E+00	1.80E+00	1.93E+00	2.63E+00	1.48E+00	1.07E-03	8.30E-04	8.23E-04	8.97E-04	8.31E-04	1.21E-03	9.95E-04	1.47E-03
		$WL = -0.4491(BP_a) + 43.514$	0.8347																	

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	Barometric Efficiency	Trend Equation[1]	R^2	BP Correction Applied? (Y/N)	Transmissivity (ft^2/min)								Storativity							
					Leaky - Hantush-Jacob - no storage	*Leaky - Hantush-Jacob - storage*	*Leaky - Moench (Case 1)*	*Leaky - Moench (Case 2)*	*Leaky - Neuman Witherspoon*	*Confined - Thesis*	*Confined - Papadopulos-Cooper*	*Confined - Cooper-Jacobs*	*Leaky - Hantush-Jacob - no storage*	*Leaky - Hantush-Jacob - storage*	*Leaky - Moench (Case 1)*	*Leaky - Moench (Case 2)*	*Leaky - Neuman Witherspoon*	*Confined - Thesis*	*Confined - Papadopulos-Cooper*	*Confined - Cooper-Jacobs*
CH-16	0	-	-																	
CH-5	71.7% (Ave.)	$WL = -0.705(BP_a) + 106.95$	0.6682	Y	Not Analyzed; doesn't seem to be responding to pump test															
		$WL = -0.7281(BP_a) + 107.76$	0.7163																	
CH-9	59.4%	$WL = -0.6086(BP_a) + 264.94$	0.6491	Y	3.17E+00	4.18E+00	2.79E+00	4.21E+00	4.77E+00	4.46E+00	4.46E+00	3.60E+00	4.10E-03	3.80E-03	4.58E-03	2.95E-03	3.73E-03	4.66E-03	3.96E-03	3.15E-03
		$WL = -0.5795(BP_a) + 263.93$	0.465																	
CH-19	-	$WL = 0.021(BP_a) + 205.19$	0.0049	N	1.25E+01	1.32E+01	1.11E+01	1.59E+01	1.21E+01	1.98E+01	2.23E+01	3.60E+00	5.35E-03	3.06E-03	1.98E-03	4.00E-03	2.84E-03	2.39E-03	3.35E-03	3.15E-03
MW-121	90.5%	$WL = -0.905(BP_a) + 90.059$	0.6563	Y	6.21E+00	6.46E+00	6.54E+00	4.22E+00	1.24E+00	6.44E+00	6.71E+00	1.95E+00	9.84E-04	9.62E-04	1.07E-03	7.07E-04	3.88E-05	7.88E-04	1.61E-03	4.18E-03
MW-43	23.1% (Ave.)	$WL = -0.2276(BP_a) + 18.72$	0.6367	Y	Not Analyzed; doesn't seem to be responding to pump test															
		$WL = -0.1607(BP_a) + 16.408$	0.6735																	
MW-55	-	$WL = -0.673(BP_a) + 35.074$	0.1257	N	1.72E+00	1.50E+00	3.31E+00	2.48E+00	1.32E+00	1.52E+00	1.49E+00	6.27E-01	1.58E-03	2.42E-03	2.73E-03	2.26E-03	2.38E-03	2.03E-03	2.02E-03	2.48E-03
		$WL = -0.0971(BP_a) + 15.325$	0.0019																	
MW-57	35.2% (Ave.)	$WL = -0.3556(BP_a) + 17.948$	0.7164	Y	Poor	Poor	Poor	Poor	Poor	Poor	Poor	9.33E-01	Poor	Poor	Poor	Poor	Poor	Poor	Poor	1.42E-04
		$WL = -0.2487(BP_a) + 14.26$	0.7350																	
		$WL = -0.4534(BP_a) + 21.286$	0.7284																	
MW-70-1	-	$WL = -0.1798(BP_a) + 33.943$	0.4328	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-103A	-	$WL = -0.112(BP_a) + 10.57$	0.2459	N	Not Analyzed; doesn't seem to be responding to pump test															
MW-103B	38.7% (Ave.)	$WL = -0.3526(BP_a) + 44.928$	0.6477	Y	6.70E+00	8.79E+00	8.73E+00	7.50E+00	7.48E+00	9.99E+00	8.12E+00	4.84E+00	4.04E-03	3.76E-03	3.47E-03	2.64E-03	3.42E-03	3.44E-03	3.74E-03	6.43E-03
		$WL = -0.3244(BP_a) + 43.931$	0.6209																	
		$WL = -0.4847(BP_a) + 49.437$	0.6756																	
MW-104A	47.7%	$WL = -0.4772(BP_a) + 21.341$	0.7334	Y	8.19E+00	7.50E+00	7.50E+00	4.09E+00	1.19E+00	7.47E+00	7.45E+00	4.12E+00	6.11E-03	6.28E-03	6.28E-03	3.64E-03	1.13E-03	6.29E-03	6.32E-03	5.83E-03
MW-104B	-	$WL = 1.0843(BP_a) - 9.8875$	0.8916	N	3.22E+00	3.15E+00	3.82E+00	3.64E+00	3.08E+00	2.79E+00	3.79E+00	2.27E+00	1.73E-03	1.45E-03	9.59E-04	1.46E-03	7.47E-04	1.66E-03	1.64E-03	2.21E-03
MW-105B	40.6%	$WL = -0.3528(BP_a) + 46.291$	0.6331	Y	9.72E+00	1.03E+01	9.52E+00	7.86E+00	1.43E+00	9.90E+00	9.27E+00	4.57E+00	3.53E-03	3.21E-03	3.69E-03	2.82E-03	2.75E-04	3.26E-03	3.46E-03	5.01E-03
		$WL = -0.3621(BP_a) + 46.574$	0.6900																	
		$WL = -0.504(BP_a) + 51.451$	0.6782																	
MW-106A	47.7%	$WL = -0.4772(BP_a) + 21.341$	0.7334	Y	5.02E+00	4.95E+00	4.48E-01	3.79E+00	5.83E+00	5.03E+00	4.72E+00	3.04E+00	1.00E-10	1.00E-10	2.94E-11	1.00E-10	1.00E-10	1.00E-10	1.00E-10	1.03E-10
MW-106B	-	$WL = .6847(BP_a) + 3.997$	0.8169	N	1.87E+00	1.06E+00	1.45E+00	1.11E+00	1.25E+00	1.55E+00	2.02E+00	2.50E+00	8.29E-03	5.34E-03	5.58E-03	6.20E-03	4.30E-03	8.95E-03	7.68E-03	5.00E-03
MW-107	69.5%	$WL = -0.6953(BP_a) + 47.671$	0.7026	Y	1.86E+00	4.03E-01	4.88E-01	1.13E+00	1.68E+00	1.68E+00	1.68E+00	1.81E+00	2.21E-03	4.61E-04	3.61E-04	7.02E-03	3.81E-03	3.81E-03	3.81E-03	2.62E-03
MW-108A	>1	Spike in WL at 5/27 18:51	-	N	Not Analyzed; XD movement															
MW-108B	83.6%	$WL = -0.8324(BP_a) + 54.281$	0.7055	Y	2.73E+00	2.72E+00	2.73E+00	2.72E+00	Poor	2.72E+00	2.72E+00	1.49E+00	1.89E-03	1.89E-03	1.90E-03	1.72E-03	Poor	1.89E-03	1.89E-03	1.68E-03
		$WL = -0.8474(BP_a) + 54.788$	0.7280																	

1) 5/23/2010 @ 3pm to 5/24/2010 @ 3pm

Poor fit
Best fit
Not Analyzed with Note

confirmed correct values
corrected value inserted

TABLE 12 SUMMARY OF AQUIFER CHARACTERISTICS DETERMINED BY PUMP TEST DATA ANALYSIS

ZONE 1 WELLS

Well ID	Well Type	Uncorrected DD Plot	Baro Eff Evaluation	Corrected DD Plot	
CH-7	Corehole	X	X	X	
CH-13	Corehole	X	X	X	Apparent WL manipulations during post-pump static
CH-14	Corehole	X	X	X ?-ah	
CH-16	Pumping	X	X	X	Pumping well - semi log plot looks odd
CH-18	Corehole	X	X	X	
CH-20	Corehole	X	X	X	
MW-115	Deep Obs	X	X		?????
MW-116	Deep Obs	X	X	X	
MW-118	Deep Obs	X	X	X	
MW-120	Deep Obs	X	X	X	
MW-122	Deep Obs	X	X	X	
MW-12	Existing Bedrock	X	X	X	No apparent response to pumping - late rise in WL
MW-39A	Existing Bedrock	X	X	X	No apparent response to pumping
MW-40A	Existing Bedrock	X	X	X	No apparent response to pump stop
MW-41	Existing Bedrock	X	X	X	Very similar to CH-2
MW-34	Existing Bedrock	X	X	X	Very similar to CH-2
MW-35	Existing Bedrock	X	X	X	Very similar to CH-2
MW-36	Existing Bedrock	X	X	X	Very similar to CH-2
MW-46	Existing Bedrock	X	X	X	
MW-10	straddle?	X	X	X	
MW-42	straddle?	X	X	X	No apparent response to pumping need to adjust for XD movement
MW-19A	straddle?	X	X	X	

ZONE 2 WELLS

Well ID	Well Type				
CH-2	Corehole	X	X	X	Weak apparent response to pump stop
CH-3	Corehole	X	X	X	No apparent response to pumping need to adjust for XD movement
CH-4	Corehole	X	X		Very similar to CH-2
CH-6	Corehole	X	X	X	No response to pumping odd WL spike same timing as that in MW-12
CH-8	Corehole	X	X	X	Very similar to CH-2
CH-10	Corehole	X	X	X	
CH-11	Corehole	X	X	X	
CH-12	Corehole	X	X	X	
MW-113	Deep Obs	X	X	X	
MW-114	Deep Obs	X	X	X	
MW-2	Existing Bedrock	X	X	X	No apparent response to pumping, odd WL spike same timing as MW-12
MW-3	Existing Bedrock	X	X	X	No apparent response to pump stop, need to adjust for XD movement
MW-24	Existing Bedrock	X	X	X	Very similar to CH-2
MW-37	Existing Bedrock	X	X	X	No apparent response to pumping, odd WL spike same timing as MW-12
MW-59	Existing Bedrock	X	X	X	No apparent response to pumping need to adjust for XD movement
MW-61	Existing Bedrock	X	X	X	No apparent response to pumping need to adjust for XD movement

ZONE 3 WELLS

Well ID	Well Type				
CH-1	Corehole	X	X	X	Y-axis is incorrect, need to adjust for XD movement
CH-15	Corehole	X	X	X	
CH-17	Corehole	X	X	X	
MW-117	Deep Obs	X	X	X	
MW-119	Deep Obs	X	X	X	
MW-5	Existing Bedrock	X	X	X	No apparent response to pumping
MW-6A	Existing Bedrock	X	X	X	No apparent response to pumping
MW-7C	Existing Bedrock	X	X	X	Very similar to CH-2
MW-8A	Existing Bedrock	X	X	X	Need to adjust for XD movement
MW-15B	Existing Bedrock	X	X	X	No response to pump stop
MW-22A	Existing Bedrock	X	X	X	Very similar to CH-2
MW-26A	Existing Bedrock	X	X	X	
MW-50	Existing Bedrock	X	X	X	Very similar to CH-2
MW-52	Existing Bedrock	X	X	X	Very similar to CH-2
MW-63	Existing Bedrock	X	X	X	
MW-74	Existing Bedrock	X	X	X	

ZONE 4 WELLS

Well ID	Well Type				
CH-5	Corehole	X	X	X	Questionable response to pumping
CH-9	Corehole	X	X	X	Semi log of DD starts neg
CH-19	Corehole	X	X	X	
MW-121	Deep Obs	X	X	X	
MW-43	Existing Bedrock	X	X	X	No apparent response to pumping
MW-55	Existing Bedrock	X	X	X	Not an obvious response to pumping
MW-57	Existing Bedrock	X	X	X	
MW-70-1	Existing Bedrock	X	X	X	No apparent response to pumping
MW-103B	Existing Bedrock	X	X	X	Very similar to CH-2
MW-104B	Existing Bedrock	X	X	X	Response to pump stop somewhat delayed
MW-105B	Existing Bedrock	X	X	X	Very similar to CH-2
MW-106B	Existing Bedrock	X	X	X	Weak apparent response to pump stop
MW-107	Existing Bedrock	X	X	X	
MW-108B	Existing Bedrock	X	X	X	